

UNIVERSITY OF SWAZILAND

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FACULTY OF SCIENCE

DEPARTMENT OF PHYSICS

SUPPLEMENTARY EXAMINATION 2010/2011

TITLE OF PAPER : ELECTROMAGNETIC THEORY I

COURSE NUMBER : P331

TIME ALLOWED : THREE HOURS

INSTRUCTIONS : ANSWER ANY FOUR OUT OF FIVE
QUESTIONS.
EACH QUESTION CARRIES 25 MARKS.

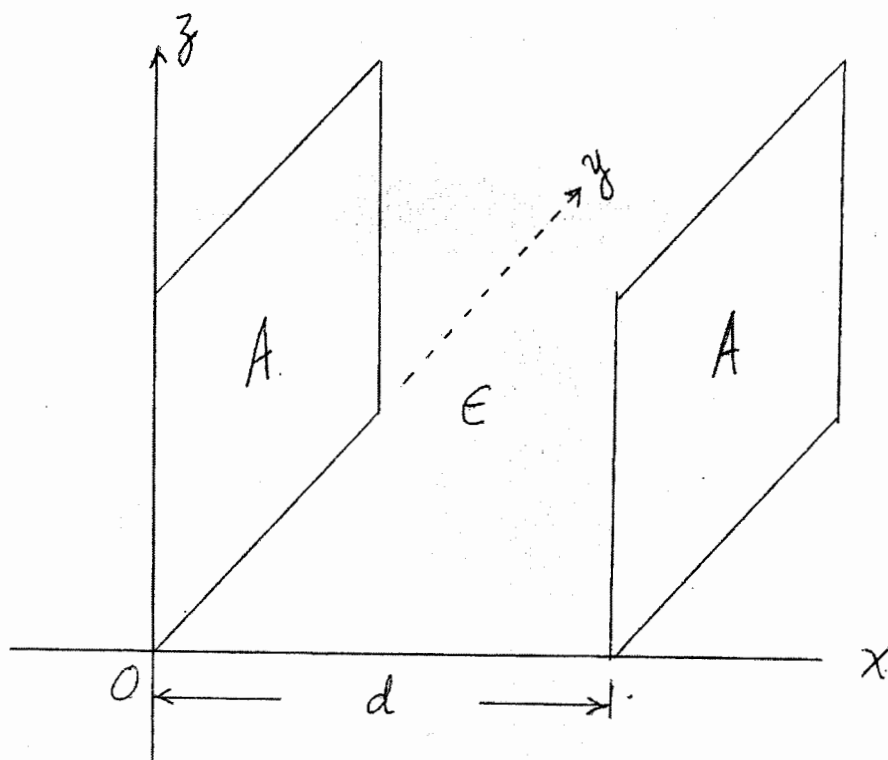
MARKS FOR DIFFERENT SECTIONS ARE
SHOWN IN THE RIGHT-HAND MARGIN.

THIS PAPER HAS NINE PAGES, INCLUDING THIS PAGE.

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Question one

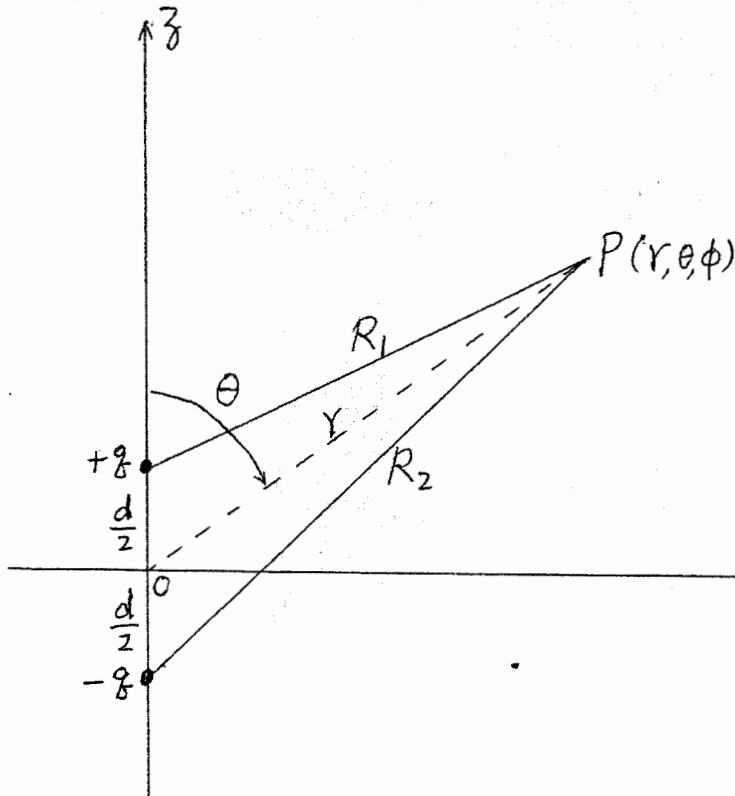
- (a) For a two-parallel conducting plate capacitor system as shown in the following diagram



where A is the plate surface area, d is the plate separation and ϵ is the dielectric constant of the insulating material layer in-between the two plates.

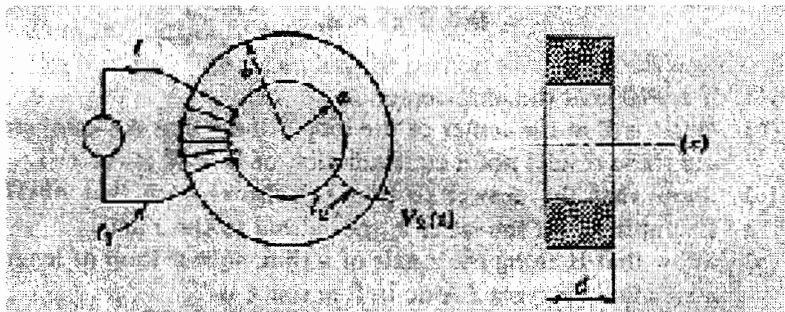
- (i) From $\nabla^2 f(x) = 0$ with boundary conditions of $f(x=0) = 0$ and $f(x=d) = V_0$, find the specific solution of $f(x)$, (4 marks)
- (ii) find \vec{E} from $f(x)$ obtained in (a)(i), (3 marks)
- (iii) find ρ_s on $x=0$ and $x=d$ respectively. Then find the total charges on both surfaces with surface area A and show that they are equal and opposite. (5 marks)

- (b) For an electric dipole situated at the origin, i.e., $+q$ situated at $z = \frac{d}{2}$ & $-q$ situated at $z = -\frac{d}{2}$ along z -axis, the electric potential Φ at the space point $P:(r, \theta, \phi)$ due to this dipole is $\Phi = \Phi_1 + \Phi_2$ where $\Phi_1 = \frac{+q}{4\pi\epsilon_0 R_1}$ and $\Phi_2 = \frac{-q}{4\pi\epsilon_0 R_2}$, as depicted in the following diagram



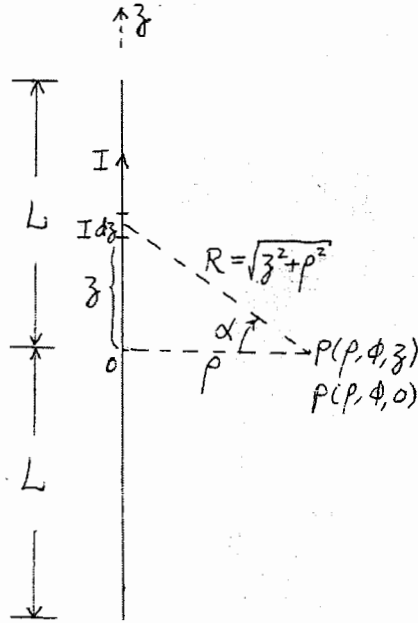
- (i) for $r \gg d$, use $R_1 \approx r - \frac{d}{2} \cos(\theta)$ and $R_2 \approx r + \frac{d}{2} \cos(\theta)$, deduce that $\Phi \approx \frac{p \cos(\theta)}{4\pi\epsilon_0 r^2}$ where $p = qd$ is the electric dipole moment. (7 marks)
- (ii) from Φ in (b)(i), deduce that the electric field at far away point from the electric dipole source situated at the origin given in the above diagram is $\vec{E} = \frac{p}{4\pi\epsilon_0 r^3} (\vec{e}_r 2 \cos(\theta) + \vec{e}_\theta \sin(\theta))$ (6 marks)

- (a) A static current I flows in the n_1 turn toroid l_1 wiring around a iron ring core of magnetic permeability μ with the rectangular cross-section area $(b - a) \times d$ as shown below



- (i) use integral Ampere's law, choose proper closed loops to find \vec{B} in terms of ρ , n_1 , μ & I within the iron core, i.e., $a \leq \rho \leq b$ & $0 \leq z \leq d$ region, (7 marks)
- (ii) find the total magnetic flux Ψ_m passing through the cross-section area $(b - a) \times d$ of the iron ring in counter clockwise sense, i.e., $\int_S \vec{B} \cdot d\vec{s}$ where $S: a \leq \rho \leq b$, $0 \leq z \leq d$ & $d\vec{s} = \vec{a}_\phi d\rho dz$, in terms of a, b, d, n_1, μ & I . (6 marks)
- (iii) find the external self-inductance L_e of the toroid wire l_1 in terms of a, b, d, μ & n_1 . (3 marks)
- (b) Placing a single turn secondary coil l_2 around the iron ring, if the toroid wire l_1 carries a sinusoidal current of $I_0 \sin(\omega t)$ instead of carrying a static current I , find the induced e.m.f. $V_2(t)$ for a single turn secondary coil l_2 in terms of $a, b, d, \omega, n_1, \mu$ & I_0 under quasi static situation. If $a = 7 \text{ cm}$, $b = 10 \text{ cm}$, $d = 2 \text{ cm}$, $n_1 = 100$, $f = 300 \text{ Hz}$, $\mu = 4000 \mu_0$ and $I_0 = 2 \text{ A}$, compute the amplitude of $V_2(t)$. (9 marks)

- (a) For the time-independent (or static) case, setting $\vec{B} = \vec{\nabla} \times \vec{A}$ and using Coulomb's gauge, i.e., $\vec{\nabla} \cdot \vec{A} = 0$, to deduce the following Poisson's equations for \vec{A} from Maxwell's equations as $\nabla^2 \vec{A} = -\mu \vec{J}$. (5 marks)
- (b) A straight thin conducting wire of length $2L$ carries a total current I along $+z$ direction as shown in the diagram below:



- (i) find the z -component of vector potential \vec{A} , i.e., A_z , due to the above given current at a point $P: (\rho, \phi, 0)$ by evaluating the following integral

$$A_z = \int_{z=-L}^L \frac{\mu_0 I dz}{4\pi R} = 2 \int_{z=0}^L \frac{\mu_0 I dz}{4\pi \sqrt{z^2 + \rho^2}} \quad \text{and show that}$$

$$A_z = \frac{\mu_0 I}{2\pi} \left(\ln \left(\frac{\sqrt{\rho^2 + L^2} + L}{\rho} \right) \right) \quad (10 \text{ marks})$$

(Hint: $d \tan(\alpha) = \sec^2(\alpha) d\alpha$ & $1 + \tan^2(\alpha) = \sec^2(\alpha)$,
 $\int \sec(\alpha) d\alpha = \ln(\sec(\alpha) + \tan(\alpha))$)

- (ii) From $\vec{B} = \vec{\nabla} \times \vec{A}$ and knowing $A_\rho = 0 = A_\phi$, find the magnetic field \vec{B} at the point P due to the above given current. In the case of $L \gg \rho$, show that magnetic field \vec{B} obtained here can be simplified to $\vec{B} = \vec{a}_\phi \frac{\mu_0 I}{2\pi \rho}$. (10 marks)

- (a) Starting with the following time harmonic Maxwell's equations for a material region represented by parameters of μ , ϵ & σ as

$$\vec{\nabla} \cdot \vec{\tilde{E}}(\vec{r}) = 0 \quad \dots\dots (1)$$

$$\vec{\nabla} \cdot \vec{\tilde{H}}(\vec{r}) = 0 \quad \dots\dots (2)$$

$$\vec{\nabla} \times \vec{\tilde{E}}(\vec{r}) = -i \omega \mu \vec{\tilde{H}}(\vec{r}) \quad \dots\dots (3)$$

$$\vec{\nabla} \times \vec{\tilde{H}}(\vec{r}) = (\sigma + i \omega \epsilon) \vec{\tilde{E}}(\vec{r}) \quad \dots\dots (4)$$

and further assuming that $\vec{\tilde{E}}(\vec{r})$ & $\vec{\tilde{H}}(\vec{r})$ are functions of z only, i.e.,

$$\vec{\tilde{E}}(\vec{r}) = \vec{a}_x \hat{E}_x(z) + \vec{a}_y \hat{E}_y(z) + \vec{a}_z \hat{E}_z(z) \quad \dots\dots (5)$$

$$\vec{\tilde{H}}(\vec{r}) = \vec{a}_x \hat{H}_x(z) + \vec{a}_y \hat{H}_y(z) + \vec{a}_z \hat{H}_z(z) \quad \dots\dots (6)$$

deduce that $\hat{E}_z(z) = 0 = \hat{H}_z(z)$ and

$$\frac{d^2 \hat{E}_x(z)}{dz^2} = -\hat{\gamma}^2 \hat{E}_x(z) \quad \text{where} \quad \hat{\gamma} = \sqrt{(\omega^2 \mu \epsilon - i \omega \mu \sigma)} \quad , \quad (12 \text{ marks})$$

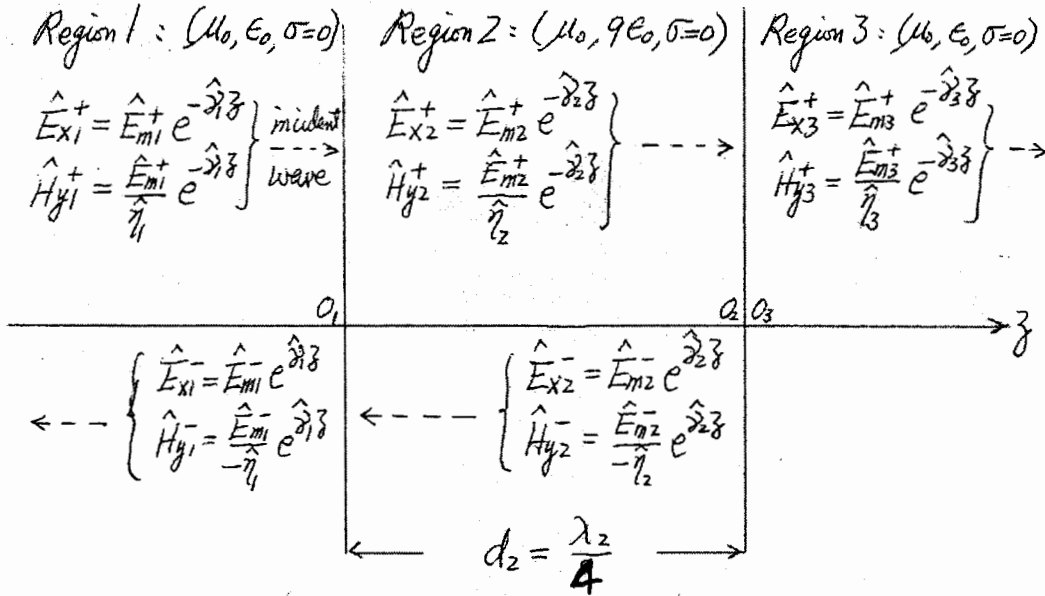
- (b) An uniform plane wave travelling along $+z$ direction with the field components of (E_x, H_y) has a complex electric field amplitude of $80 e^{i40^\circ} \frac{V}{m}$ and propagates at $f = 6 \times 10^7 \text{ Hz}$ in a material region having the parameters of $\mu = \mu_0$, $\epsilon = 4 \epsilon_0$ & $\frac{\sigma}{\omega \epsilon} = 0.6$,

- Find the values of the propagation constant $\hat{\gamma} (= \alpha + i \beta)$ and the intrinsic wave impedance $\hat{\eta}$ for this wave. (5 marks)
- express the electric and magnetic fields in both their complex and real-time forms, with the numerical values of (b)(i) inserted, (5 marks)
- find the values of the penetration depth, wave length and phase velocity of the given wave. (3 marks)

Question five

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An uniform plane wave $(\hat{E}_{x1}^+, \hat{H}_{y1}^+)$, operates at $f = 10^8$ Hz, is normally incident upon a lossless layer of $d_2 \left(= \frac{\lambda_2}{4} \right)$ thickness with parameters of $(\mu = \mu_0, \epsilon = 9 \epsilon_0)$ as shown below :



0_1 , 0_2 & 0_3 are the respective origins for region 1, 2 & 3 chosen at the first and second interface. (Both region 1 and region 3 are air region.)

- (a) Define for the i^{th} region ($i = 1, 2, 3$) the reflection coefficient $\hat{\Gamma}_i(z)$ and the total wave impedance $\hat{Z}_i(z)$ and deduce the following :

$$\left\{ \begin{array}{l} \hat{Z}_i(z) = \hat{\eta}_i \frac{1 + \hat{\Gamma}_i(z)}{1 - \hat{\Gamma}_i(z)} \quad \text{and reversely} \quad \hat{\Gamma}_i(z) = \frac{\hat{Z}_i(z) - \hat{\eta}_i}{\hat{Z}_i(z) + \hat{\eta}_i} \quad \text{and} \\ \hat{\Gamma}_i(z') = \hat{\Gamma}_i(z) e^{2\hat{\gamma}_i(z'-z)} \quad \text{where } z' \text{ \& } z \text{ are two points in } i^{th} \text{ region} \end{array} \right. \quad (10 \text{ marks})$$

- (b) (i) find the values of $\hat{\gamma}_1$, $\hat{\gamma}_2$, $\hat{\gamma}_3$, $\hat{\eta}_2$ & λ_2 , (note: $\hat{\eta}_1 = \hat{\eta}_3 = 120 \pi \Omega$ and $\alpha_1 = \alpha_2 = \alpha_3 = 0$) (3 marks)
- (ii) starting with $\hat{\Gamma}_3(z) = 0$ for the rightmost region, i.e., region 3, and using continuous \hat{Z} at the interface as well as the equations in (a), find the values of $\hat{Z}_3(0)$, $\hat{Z}_2(0)$, $\hat{\Gamma}_2(0)$, $\hat{\Gamma}_2(-d_2)$, $\hat{Z}_2(-d_2)$, $\hat{Z}_1(0)$ & $\hat{\Gamma}_1(0)$ (10 marks)
- (iii) find the value of \hat{E}_{m1}^- if given $\hat{E}_{m1}^+ = 50 e^{i40^\circ} \frac{V}{m}$ (2 marks)

$$e = 1.6 \times 10^{-19} \text{ C}$$

$$m_e = 9.1 \times 10^{-31} \text{ kg}$$

$$\mu_0 = 4 \pi \times 10^{-7} \frac{\text{H}}{\text{m}}$$

$$\varepsilon_0 = 8.85 \times 10^{-12} \frac{\text{F}}{\text{m}}$$

$$\alpha = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} - 1}$$

$$\beta = \frac{\omega \sqrt{\mu \varepsilon}}{\sqrt{2}} \sqrt{\sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} + 1}$$

$$\frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 3 \times 10^8 \frac{\text{m}}{\text{s}}$$

$$\hat{\eta} = \frac{\sqrt{\frac{\mu}{\varepsilon}}}{\sqrt[4]{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2}} e^{i \frac{1}{2} \tan^{-1}\left(\frac{\sigma}{\omega \varepsilon}\right)}$$

$$\eta_0 = 120 \pi \quad \Omega = 377 \quad \Omega$$

$$\beta_0 = \omega \sqrt{\mu_0 \varepsilon_0}$$

$$\oint_S \vec{E} \cdot d\vec{s} = \frac{1}{\varepsilon} \iiint_V \rho_v dv$$

$$\oint_S \vec{B} \cdot d\vec{s} = 0$$

$$\oint_L \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \left(\iint_S \vec{B} \cdot d\vec{s} \right)$$

$$\oint_L \vec{B} \cdot d\vec{l} = \mu \iint_S \vec{J} \cdot d\vec{s} + \mu \varepsilon \frac{\partial}{\partial t} \left(\iint_S \vec{E} \cdot d\vec{s} \right)$$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho_v}{\varepsilon}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{J} + \mu \varepsilon \frac{\partial \vec{E}}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\oint_S \vec{F} \cdot d\vec{s} = \iiint_V (\vec{\nabla} \cdot \vec{F}) dV \quad \text{divergence theorem}$$

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$$\oint_L \vec{F} \cdot d\vec{l} = \iint_S (\vec{\nabla} \times \vec{F}) \cdot d\vec{s} \quad \text{Stokes' theorem}$$

$$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{F}) = 0$$

$$\vec{\nabla} \times (\vec{\nabla} f) = 0$$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{F}) = \vec{\nabla} (\vec{\nabla} \cdot \vec{F}) - \nabla^2 \vec{F}$$

$$\begin{aligned} \vec{\nabla} f &= \vec{e}_x \frac{\partial f}{\partial x} + \vec{e}_y \frac{\partial f}{\partial y} + \vec{e}_z \frac{\partial f}{\partial z} = \vec{e}_\rho \frac{\partial f}{\partial \rho} + \vec{e}_\phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + \vec{e}_z \frac{\partial f}{\partial z} \\ &= \vec{e}_r \frac{\partial f}{\partial r} + \vec{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \vec{e}_\phi \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi} \end{aligned}$$

$$\begin{aligned} \vec{\nabla} \cdot \vec{F} &= \frac{\partial(F_x)}{\partial x} + \frac{\partial(F_y)}{\partial y} + \frac{\partial(F_z)}{\partial z} = \frac{1}{\rho} \frac{\partial(F_\rho \rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial(F_\phi)}{\partial \phi} + \frac{\partial(F_z)}{\partial z} \\ &= \frac{1}{r^2} \frac{\partial(F_r r^2)}{\partial r} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\theta \sin(\theta))}{\partial \theta} + \frac{1}{r \sin(\theta)} \frac{\partial(F_\phi)}{\partial \phi} \end{aligned}$$

$$\begin{aligned} \vec{\nabla} \times \vec{F} &= \vec{e}_x \left(\frac{\partial(F_z)}{\partial y} - \frac{\partial(F_y)}{\partial z} \right) + \vec{e}_y \left(\frac{\partial(F_x)}{\partial z} - \frac{\partial(F_z)}{\partial x} \right) + \vec{e}_z \left(\frac{\partial(F_y)}{\partial x} - \frac{\partial(F_x)}{\partial y} \right) \\ &= \frac{\vec{e}_\rho}{\rho} \left(\frac{\partial(F_z)}{\partial \phi} - \frac{\partial(F_\phi \rho)}{\partial z} \right) + \vec{e}_\phi \left(\frac{\partial(F_\rho)}{\partial z} - \frac{\partial(F_z)}{\partial \rho} \right) + \frac{\vec{e}_z}{\rho} \left(\frac{\partial(F_\phi \rho)}{\partial \rho} - \frac{\partial(F_\rho)}{\partial \phi} \right) \\ &= \frac{\vec{e}_r}{r^2 \sin(\theta)} \left(\frac{\partial(F_\phi r \sin(\theta))}{\partial \theta} - \frac{\partial(F_\theta r)}{\partial \phi} \right) + \frac{\vec{e}_\theta}{r \sin(\theta)} \left(\frac{\partial(F_r)}{\partial \phi} - \frac{\partial(F_\phi r \sin(\theta))}{\partial r} \right) + \frac{\vec{e}_\phi}{r} \left(\frac{\partial(F_\theta r)}{\partial r} - \frac{\partial(F_r)}{\partial \theta} \right) \end{aligned}$$

where $\vec{F} = \vec{e}_x F_x + \vec{e}_y F_y + \vec{e}_z F_z = \vec{e}_\rho F_\rho + \vec{e}_\phi F_\phi + \vec{e}_z F_z = \vec{e}_r F_r + \vec{e}_\theta F_\theta + \vec{e}_\phi F_\phi$ and

$d\vec{l} = \vec{e}_x dx + \vec{e}_y dy + \vec{e}_z dz = \vec{e}_\rho d\rho + \vec{e}_\phi \rho d\phi + \vec{e}_z dz = \vec{e}_r dr + \vec{e}_\theta r d\theta + \vec{e}_\phi r \sin(\theta) d\phi$

$$\begin{aligned} \nabla^2 f &= \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2} \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin(\theta)} \frac{\partial}{\partial \theta} \left(\sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2(\theta)} \frac{\partial^2 f}{\partial \phi^2} \end{aligned}$$